

# Mass lumping and

quadrature formulas

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# Model problem

1D wave equation:

$$\partial_{tt} u - \partial_{xx} u = 0$$

$$u(x, 0) = u_0(x)$$

$$\partial_t u(x, 0) = u_1(x)$$

$$\text{in } \mathbb{R} : u(x, t) = u_0(x+t) + u_0(x-t) + \frac{1}{2} \int_{x-t}^{x+t} u_1(s) ds$$

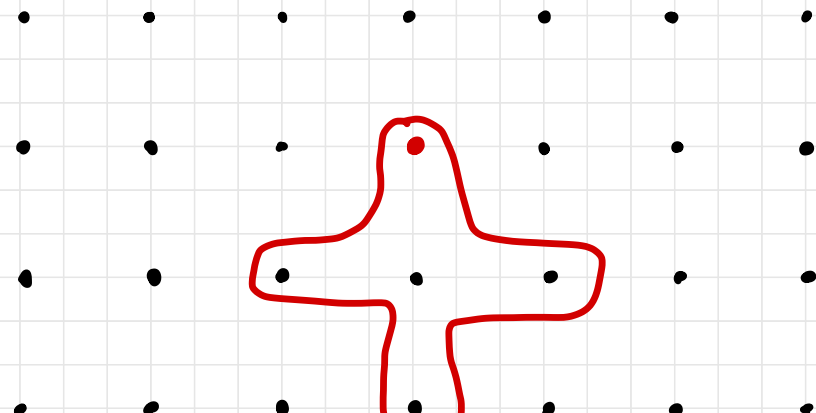
on  $[a, b]$ :  $u(x, t) = \dots$  numerical methods instead!  $\nabla$   
or RHS  
FD, FEM, ...

# Finite differences

$$u_{tt} - u_{xx} = 0 \quad \rightsquigarrow$$

$$\frac{u_x^{n+1} - 2u_x^n + u_x^{n-1}}{\tau^2} = \frac{u_{x-1}^n - 2u_x^n + u_{x+1}^n}{h^2}$$

$\tau$  {



- higher order methods lead to larger stencils
- boundary conditions?

# Finite element method

Find  $(u_h^n)_n \in V_h$

$$\left( \frac{u_h^{n+1} - 2u_h^n + u_h^{n-1}}{\tau^2}, v_h \right) + (\partial_x u_h^n, \partial_x v_h) = 0, \quad \forall v_h \in V_h$$

For a  $V_h$  and a set of basis functions, we get

mass  
matrix

$M$

$$\frac{u^{n+1} - 2u^n + u^{n-1}}{\tau^2}$$

stiffness  
matrix.

$K$

$$u^n = 0$$

What do we know about  $M$ ?

Would be nice if it were easy to invert...

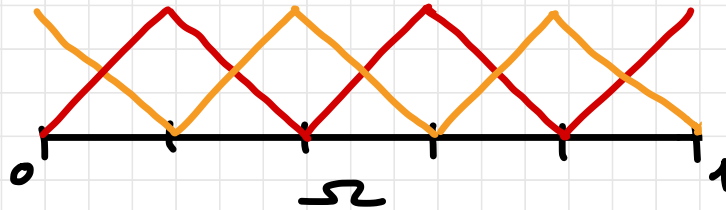
$$u^{n+1} = 2u^n - u^{n-1} + \tau^2 M^{-1} K u^n$$



**Mass lumping** : replace  $M$  by an approx  $M_h$

- Idea : row-sum of  $M$ , i.e.  $M_h := \text{diag}(\text{sum}(M))$ 
  - Pro :  $M_h$  is diagonal
  - Con : **NO ANALYSIS**

- Idea #2 : use numerical quadrature



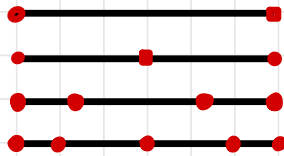
$$(M_h)_{ij} = \sum_{T \in \mathcal{T}_h} \int_T \phi_j \phi_i = \int_{T^*} \phi_j \phi_i = \delta_{ij} \cdot |T^*| \cdot \frac{1}{2}$$



## Higher order mass lumping in 1D

Let  $V_h = P_k(T_h) \cap H^1(\Omega)$ . A few remarks:

- For continuity reasons, we "must" include the vertices as quadrature points.  $\hookrightarrow$  Gauss-Lobatto



GL with  $k+1$  points integrate all  $P_{2k-1}$  exactly

- $\dim P_k = k+1$
- Lumped mass matrix  $M_h$  is diagonal, no loss of convergence due to mass lumping



## Wave equation 2D/3D

$$\partial_{tt} u - \Delta u = 0$$

$$u(x, 0) = u_0(x)$$

$$\partial_t u(x, 0) = u_1(x)$$

- In  $\mathbb{R}^2/\mathbb{R}^3$ :  $u(x, t) = \dots$  "Kirchhoff's formulas"
- On bounded domains / inhomogeneous right-hand sides:  
 $u(x, t) = \dots$  numerical methods instead!  $\nabla$

FD, FEM, ...

more flexible, allows for triangular grids, ...

## Wave equation 2D/3D

$$\partial_{tt} u - \Delta u = 0$$

$$u(x, 0) = u_0(x)$$

$$\partial_t u(x, 0) = u_1(x)$$

- Variational formulation: Find  $(u_h^n)_n \in V_h$

$$\left( \frac{u_h^{n+1} - 2u_h^n + u_h^{n-1}}{\tau^2}, v_h \right) + (\nabla u_h, \nabla v_h) = 0, \quad \forall v_h \in V_h$$

For a  $V_h$  and a set of basis functions, we get

mass  
matrix

$M$

$$\frac{u^{n+1} - 2u^n + u^{n-1}}{\tau^2}$$

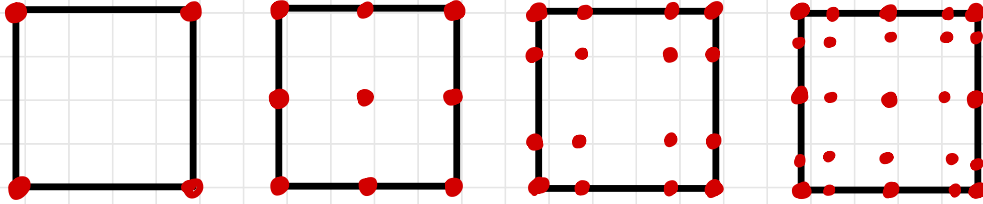
stiffness  
matrix.

$K$

$$+ K u^n = 0$$

## Mass lumping in 2D on quads

- We use tensor product Gauss-Lobatto quadrature

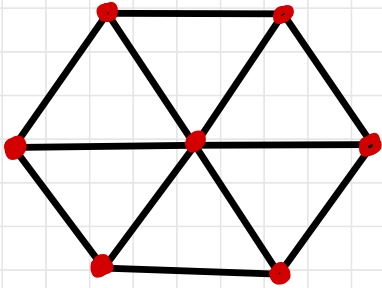


together with  $V_h = Q_k(T_h) \cap H^1(\Omega)$

- Pro: can be again constructed for arbitrary orders
- But ...  $\dim Q_k = (k+1)^2$ , while  $\dim P_k = \frac{1}{2}(k+1)(k+2)$
- What about triangles? ..

## Mass lumping in 2D on triangles

- First order: Pick  $V_h = P_1(T_h) \cap H^1(\Omega)$
- As quadrature rule, use the vertex rule

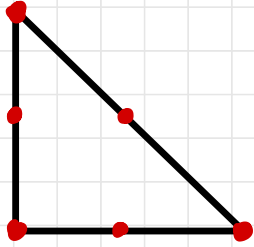


Local basis functions of the form  
 $\varphi_1(x, y) = x$ ,  $\varphi_2(x, y) = y$ ,  $\varphi_3(x, y) = 1 - x - y$

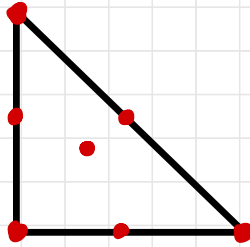
- Again, the lumped mass matrix  $M_h$  is diagonal
- What about higher orders? Gauss-Lobatto quadrature on triangles?

# Higher order mass lumping on triangles

- Second order: Pick  $V_h = P_2(T_h) \cap H^1(\Omega)$
- $\dim P_2 = 6$



only exact  
for  $P_1$



exact for  
 $P_3$  polynomials

→ but 7 quadrature  
points

- Let  $P_2^+(T) = P_2(T) + b_T$ ,  $V_h^+ := P_2^+(T_h) \cap H^1(\Omega)$
- How do we do this in general?

## Higher order mass lumping on triangles

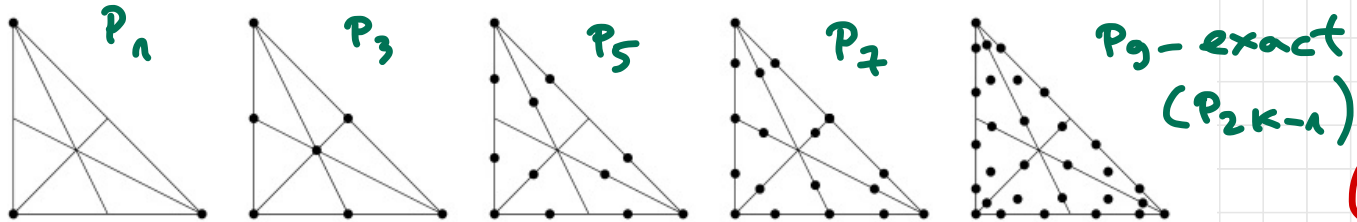
Conditions to be satisfied by the quadrature rule:

- vertices are quadrature points
- $k+1$  points on each edge (distributed symmetrically)
- positive weights (for stability of the method)
- integrates **certain** polynomials exactly

# Higher order mass lumping on triangles

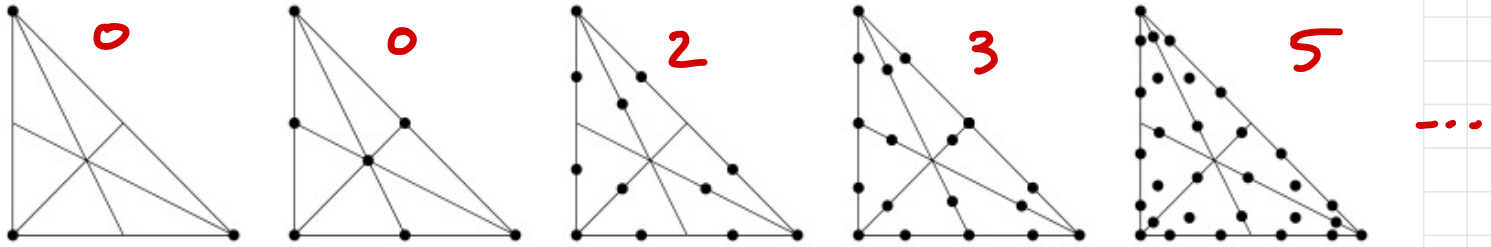
Short algorithm:

- Choose  $V_h = B_k(T_h) \cap H^1(\Omega)$ ,  $B_k(T_h) = P_k(T_h)$
  - Find a quadrature rule as described above that integrates  $k+k-2$  exactly and  $\dim B_k = \# q.p.$
  - If not possible, increase  $B_k(t) := B_k(t) + \text{bubbles}$ , new  $k$  represents the highest polynomial order.
- Go to step 2.



# Higher order mass lumping on triangles

- No systematic way of determining these quadrature rules for arbitrary orders
- Increasingly more free parameters to vary



- For any given order, solve a non-linear problem to find weights and points ... Newton
- The 3D case ... just as complicated



# Maxwell's equations

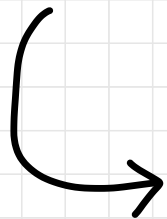
$$\partial_t E + \operatorname{curl} \operatorname{curl} E = 0 \quad \text{in } \Omega \times (0, t)$$

$$E(x, 0) = E_0 \quad \text{in } \Omega$$

$$\partial_t E(x, 0) = E_1 \quad \text{in } \Omega$$

- Variational formulation: Find  $(u_h^n)_n \in V_h \subseteq H(\operatorname{curl}, \Omega)$

$$\left( \frac{u_h^{n+1} - 2u_h^n + u_h^{n-1}}{\tau^2}, v_h \right) + (\operatorname{curl} u_h, \operatorname{curl} v_h) = 0, \quad \forall v_h \in V_h$$



mass  
matrix

$M$

$$\frac{u^{n+1} - 2u^n + u^{n-1}}{\tau^2}$$

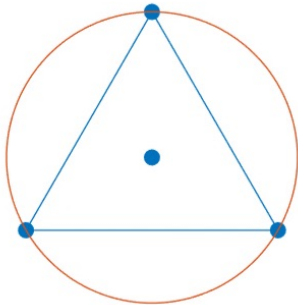
stiffness  
matrix.

$K$

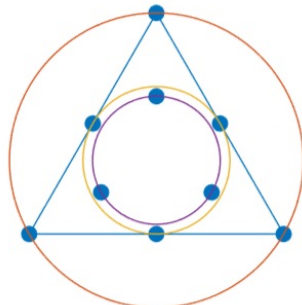
$$+ K u^n = 0$$

# Mass lumping for Maxwell's equations

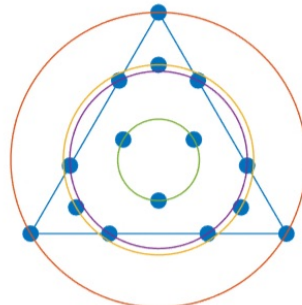
- Idea similar to  $H^1$ -conforming FEM, quadrature formulas different



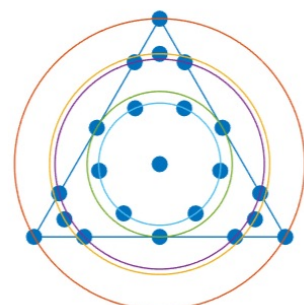
$P_2$   
(0)



$P_4$   
(1)



$P_6$   
(3)

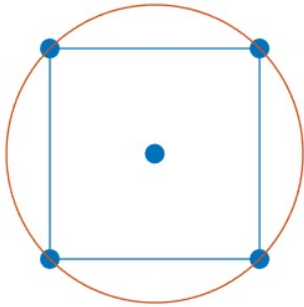


$P_8$  - exact  
(6)

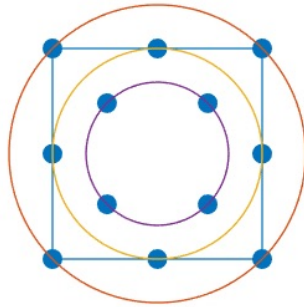
- different "sequences" of Gauss-Lobatto-type formulas

# Mass lumping for Maxwell's equations

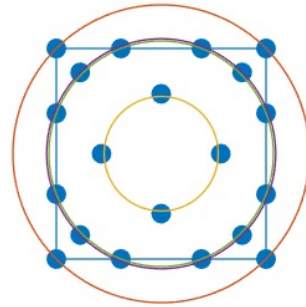
- different "sequences" of Gauss-Lobatto-type formulas  
... even on quads/hexes



$P_3$



$P_5$



$P_7$  - exact

## Takeaway

- Mass lumping is achieved by employing mass matrix approximations via quadrature rules
- No systematic way of designing arbitrary order Gauss-Lobatto quadrature formulas on simplices
- Looking towards a symbolic approach ... maybe?

