# A second order multipoint flux mixed finite element method on hybrid meshes

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Model equations for single-phase flow:



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Quantity of interest :  $\boldsymbol{p}$ 

Second order form

$$-\operatorname{div} \left( \frac{\mathbf{K} \nabla p}{p} \right) = f \qquad \text{ in } \Omega$$
$$p = 0 \qquad \text{ on } \partial \Omega.$$

- (*i*) Discontinuous schemes (DFVM), (DG) for local mass conservation
- (*ii*) Not accurate for rough coefficients (local arithmetic averaging of K)

# Porous media modeling

Model equations for single-phase flow:

Conservation of massDarcy's law $\operatorname{div} \mathbf{u} = f$  $\mathbf{u} = -K \nabla p$ 

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- (*i*) Discontinuous schemes (DFVM), (DG) for local mass conservation
- (ii) Not accurate for rough coefficients (local arithmetic averaging of K)

#### Mixed form

$$\begin{aligned} K^{-1}\mathbf{u} + \nabla p &= 0 & \text{in } \Omega \\ \text{div } \mathbf{u} &= f & \text{in } \Omega \\ p &= 0 & \text{on } \partial\Omega. \end{aligned}$$

- (*i*) Handles rough coefficients better (local harmonic averaging of *K*)
- (ii) Have to solve a full saddle point problem... or do you ?  $\Rightarrow$  MFMFE

# Variational formulation

$$\begin{split} K^{-1}\mathbf{u} + \nabla p &= 0 \qquad & \text{in } \Omega \\ & \text{div } \mathbf{u} &= f \qquad & \text{in } \Omega \\ & p &= 0 \qquad & \text{on } \partial \Omega. \end{split}$$

Variational formulation

$$(K^{-1}\mathbf{u}, \mathbf{v}) - (p, \operatorname{div} \mathbf{v}) = 0 \qquad \forall \mathbf{v} \in H(\operatorname{div}, \Omega)$$
$$(\operatorname{div} \mathbf{u}, q) = (f, q) \quad \forall q \in L^{2}(\Omega)$$

# Discrete variational formulation

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Discrete variational formulation

$$(K^{-1}\mathbf{u}_h, \mathbf{v}_h) - (p_h, \operatorname{div} \mathbf{v}_h) = 0 \qquad \forall \mathbf{v}_h \in \mathbf{V}_h \subseteq H(\operatorname{div}, \Omega)$$
$$(\operatorname{div} \mathbf{u}_h, q_h) = (f, q_h) \quad \forall q_h \in Q_h \subseteq L^2(\Omega)$$

Problem : we have to solve a full (indefinite) saddle point system ...

# Mass lumping

$$\begin{aligned} K^{-1}\mathbf{u} + \nabla p &= 0 & \text{in } \Omega \\ \text{div } \mathbf{u} &= f & \text{in } \Omega \\ p &= 0 & \text{on } \partial \Omega. \end{aligned}$$

Discrete variational formulation via mass lumping (MFMFE)

$$(K^{-1}\mathbf{u}_h, \mathbf{v}_h)_h - (p_h, \operatorname{div} \mathbf{v}_h) = 0 \qquad \forall \mathbf{v}_h \in \mathbf{V}_h \subseteq H(\operatorname{div}, \Omega)$$
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For appropriate spaces  $\mathbf{V}_h$ ,  $Q_h$  and  $(\cdot, \cdot)_h$ , the *lumped mass matrix*  $M_h$  is block-diagonal, and the variable  $\mathbf{u}_h$  can be eliminated efficiently.

$$\begin{pmatrix} \mathsf{M}_{\mathsf{h}} & -\mathsf{C}^{\top} \\ \mathsf{C} & 0 \end{pmatrix} \begin{pmatrix} \mathsf{u} \\ \mathsf{p} \end{pmatrix} = \begin{pmatrix} 0 \\ \mathsf{f} \end{pmatrix} \qquad \Longrightarrow \qquad \mathsf{C}\mathsf{M}_{\mathsf{h}}^{-1}\mathsf{C}^{\top} \mathsf{p} = \mathsf{f}$$

The problem reduces to symmetric, positive definite cell-centered system for the pressure (CCFD)

## Discretization

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M. Wheeler, I. Yotov A multipoint flux mixed finite element method. SIAM 2006  $V(T) = \mathsf{BDM}_1(T) \coloneqq P_1(T)^2 \qquad (\mathbf{u}_h, \mathbf{v}_h)_h \coloneqq \frac{|T|}{3} \sum_{i=1}^3 \mathbf{u}_h(r_i) \mathbf{v}_h(r_i)$   $Q(T) = P_0(T) \qquad r_i \text{ vertex}$ 



Figure: Matrix  $CM_h^{-1}C^T$  (left), stencil of the method (right)

## Convergence analysis

Summary of the convergence results

$$\|\mathbf{u} - \mathbf{u}_h\| = O(h)$$
 and  $\|\pi_h^0 p - p_h\| = O(h^2)$ 

Relevant properties

- (i)  $P_0(T)^2 \subseteq \mathbf{V}(T)$  and  $P_0(T) \subseteq Q(T)$  such that  $\operatorname{div} \mathbf{V}(T) \subseteq Q(T)$
- (ii)~ The quadrature rule is exact for  $P_0(T)^2 \times {\bf V}(T)$
- $(iii)~~{\rm The}~{\rm quadrature}~{\rm rule}~{\rm induces}~{\rm a}~{\rm norm}~{\rm on}~{\bf V}(T)$

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- (iii)~ The quadrature rule induces a norm on  $\mathbf{V}(T)$   $\checkmark$

Wheeler-Yotov element :  $V(T) = BDM_1(T) = P_1(T)^2$ 



Figure: DOFs of V(T) (left) and Q(T) (right). Blue circles are quadrature points. The quadrature rule is exact for  $P_1(T)$ .

Natural extension of the first order estimates

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First candidate :  $V(T) = BDM_2(T) = P_2(T)^2$ 



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- (iii)~ The quadrature rule induces a norm on  $\mathbf{V}(T)$   $\checkmark$

Second candidate :  $\mathbf{V}(T) = \mathsf{BDM}_2^+(T) = P_2(T)^2 \oplus b_3 \cdot [1,0]^T \oplus b_3 \cdot [0,1]^T$ 



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Third candidate :  $\mathbf{V}(T) = \mathsf{RT}_1(T) \coloneqq P_1(T)^2 + \mathbf{x} \cdot P_1^h(T)$ 



Figure: DOFs of V(T) (left) and Q(T) (right). Blue circles are quadrature points. The quadrature rule is exact for  $P_2(T)$ .

Split the error in  $\|\mathbf{u} - \mathbf{u}_h\|_{L^2(\Omega)} \le \|\mathbf{u} - \Pi_h \mathbf{u}\|_{L^2(\Omega)} + \|\Pi_h \mathbf{u} - \mathbf{u}_h\|_{L^2(\Omega)}$ 

$$(\Pi_h \mathbf{u} - \mathbf{u}_h, \mathbf{v}_h)_h - (\pi_h^1 p - p_h, \operatorname{div} \mathbf{v}_h) = (\Pi_h \mathbf{u} - \mathbf{u}, \mathbf{v}_h) + \sigma_h(\Pi_h \mathbf{u}, v_h)$$
$$(\operatorname{div}(\Pi_h \mathbf{u} - \mathbf{u}_h), q_h) = 0$$

with  $\sigma_h(\Pi_h \mathbf{u}, \mathbf{v}_h) = (\Pi_h \mathbf{u}, \mathbf{v}_h)_h - (\Pi_h \mathbf{u}, \mathbf{v}_h).$ 

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(I) div 
$$(\Pi_h \mathbf{u} - \mathbf{u}_h) = 0 \implies \Pi_h \mathbf{u} - \mathbf{u}_h \in P_1(T)^2$$
  
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Taking  $\mathbf{v}_h = \prod_h \mathbf{u} - \mathbf{u}_h$  and  $q_h = \pi_h^1 p - p_h$ , we obtain

$$\begin{split} \|\Pi_{h}\mathbf{u} - \mathbf{u}_{h}\|_{h}^{2} &= (\Pi_{h}\mathbf{u} - \mathbf{u}, \Pi_{h}\mathbf{u} - \mathbf{u}_{h}) + \sigma_{h}(\Pi_{h}\mathbf{u}, \Pi_{h}\mathbf{u} - \mathbf{u}_{h}) \\ &= (\Pi_{h}\mathbf{u} - \mathbf{u}, \Pi_{h}\mathbf{u} - \mathbf{u}_{h}) + \sigma_{h}(\Pi_{h}\mathbf{u} - \pi_{h}^{1}\mathbf{u}, \Pi_{h}\mathbf{u} - \mathbf{u}_{h}) \\ &\leq \|\Pi_{h}\mathbf{u} - \mathbf{u}\|_{0}\|\Pi_{h}\mathbf{u} - \mathbf{u}_{h}\|_{0} + c\|\Pi_{h}\mathbf{u} - \pi_{h}^{1}\mathbf{u}\|_{0}\|\Pi_{h}\mathbf{u} - \mathbf{u}_{h}\|_{0} \\ &\leq Ch^{2}\|\mathbf{u}\|_{H^{2}(\mathcal{T}_{h})}\|\Pi_{h}\mathbf{u} - \mathbf{u}_{h}\|_{0} \end{split}$$

#### Theorem

$$\|\mathbf{u} - \mathbf{u}_h\| = O(h^2)$$
 and  $\|\pi_h^0(p - p_h)\| = O(h^3)$ 

#### Relevant properties

- (i)  $P_1(T)^2 \subset \mathbf{V}(T)$  and  $P_1(T) \subset Q(T)$  such that  $\operatorname{div} \mathbf{V}(T) \subseteq Q(T) \checkmark$
- (*iia*)  $\exists \widetilde{\mathbf{V}}(T) \subset \mathbf{V}(T)$  s.t.  $\mathbf{v} \in \mathbf{V}(T)$  with  $\operatorname{div} \mathbf{v} \in \operatorname{div} \widetilde{\mathbf{V}}(T)$  imply  $\mathbf{v} \in \widetilde{\mathbf{V}}(T) \checkmark$
- (*ii*<sub>b</sub>) The quadrature rule is exact for  $P_1(T)^2 imes \widetilde{\mathbf{V}}(T) \checkmark$
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Third candidate :  $\mathbf{V}(T) = \mathsf{RT}_1(T) \coloneqq P_1(T)^2 + \mathbf{x} \cdot P_1^h(T)$ 



Figure: DOFs of V(T) (left) and Q(T) (right). Blue circles are quadrature points.

# Numerical tests



Figure: Snapshots of the pressure  $p_h$  (left) and the two velocity components  $u_{x,h}$ ,  $u_{y,h}$  (middle, right) for the second order approximation.

h	$DOF\ u$	DOF $p$	$\ u-u_h\ $	eoc	$\ \pi_h^0(p-p_h)\ $	eoc
$2^{-1}$	164	84	0.078309		0.033106	
$2^{-2}$	724	396	0.013097	2.57	0.002864	3.53
$2^{-3}$	2498	1386	0.002275	2.52	0.000391	2.87
$2^{-4}$	9738	5466	0.000484	2.23	0.000049	2.99
$2^{-5}$	40230	22770	0.000099	2.28	0.000005	3.13

Table: Degrees of freedom, relative discretization errors, and convergence rates for the second order multipoint flux finite element method.

# Comparison



The  $RT_1 - P_1$  pair is about 3x faster than the  $BDM_2^+ - P_1^+$  pair.

# Hybrid meshes

	dim	dim	$\ \mathbf{u} - \mathbf{u}_h\ _0$	$\ \pi_{h}^{0}p - p_{h}\ _{0}$	DOFs	DOFs
	$\mathbf{V}(T)$	Q(T)			for $\mathbf{u}_h$	for $p_h$
$BDM_1 {-} P_0$	6+0	1	O(h)	$O(h^2)$	₹ ↓	•
$RT_1-P_1$	6+2	3	$O(h^2)$	$O(h^3)$	₹ ↓	
$BDM_1 - P_0$	8+0	1	O(h)	$O(h^2)$	$\begin{array}{c} & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & $	•
$\begin{array}{c} BDFM_2 - \\ P_1 \end{array}$	8+2	3	$O(h^2)$	$O(h^3)$	$\overbrace{4}^{4}$	•

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- (iii) The theory can be used to design even higher order approximations, but finding appropriate spaces and quadrature formulas gets increasingly difficult.



Similar concept in the paper by Geevers, et al, 2018

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(iv) Application to wave propagation

$$\begin{array}{ll} \partial_t \mathbf{u} + \nabla p = f & \quad \text{in } \Omega \\ \partial_t p + \operatorname{div} \mathbf{u} = g & \quad \text{in } \Omega \\ p = 0 & \quad \text{on } \partial\Omega \end{array}$$

## Extension to poroelasicity

Poroelastic consolidation (three-field formulation)

 $K^{-1}\mathbf{u}+\nabla p=0\qquad \text{ in }\Omega$ 

$$c_s \partial_t p + \operatorname{div} \left( \alpha \partial_t \mathbf{w} \right) + \operatorname{div} \mathbf{u} = f \qquad \text{in } \Omega$$

$$-{\rm div}\left(2\mu\,\varepsilon(\mathbf{w})+\lambda\,{\rm div}\,(\mathbf{w})I\right)+\alpha\nabla p=g\qquad {\rm in}\,\,\Omega$$

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(i) The variable  $\mathbf{w}$  encodes the scructural displacement of the medium.

(ii) We can use the finite element triple  $RT_1 - P_1 - P_2^+$  with mass lumping.

$$\begin{aligned} & - D^{\top}p + M_{h} u = 0 \\ B \dot{w} + C \dot{p} &+ D u &= f \\ A w - B^{\top}p &= g \end{aligned}$$

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(iii) Algebraically, we solve the two-field formulation for p and  $\mathbf{w}$ , which is more efficient.

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- → Introduced the multipoint flux mixed finite element method (MFMFE)
- $\rightarrow$  Presented the first order approximation introduced by Wheeler and Yotov
- $\rightarrow$  Proposed an extension to second order approximations

#### H. Egger and B. Radu.

On a second-order multipoint flux mixed finite element methods on hybrid meshes. *SIAM J. Numer. Anal.*, 58(3):1822–1844, 2020.

#### A few additional remarks

- → Extension to the 3D case has also been done.
- → The framework can be used to design even higher order approximations
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- → The techniques can also be applied for the wave and Maxwell's equations

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# Thank you for your attention

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Parallelograms



(a)  $\mathsf{BDM}_1$  first order element



Tetrahedra



(a)  $BDM_1$  first order element

(b)  $RT_1$  second order element



(a) BDM<sub>1</sub> first order element





